

# **The role of waves, shelf slope and sediment characteristics on the development of erosional chenier plains**

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## **Abstract**

Cheniers are sandy ridges parallel to the coast separated by muddy deposits. Here we explore the development of erosional chenier plains, which form by winnowing during storms, through dimensional analysis and numerical results from the morphodynamic model Delft3D-SWAN. Our results show that wave energy and inner-shelf slope play an important role in the formation of erosional chenier plains. In our numerical experiments, waves affect the development of erosional chenier plains in three ways: by winnowing sand in the mudflats, by eroding mud at the shore, and by accumulating sand over the beach during extreme wave events. We further show that different sediment characteristics and wave climates lead to three alternative coastal landscapes: sandy strandplains, mudflats, or the more complex erosional chenier plains. Low inner-shelf slopes are the most favorable for mudflat and chenier plain formation, while high slopes decrease the likelihood of mudflat development and preservation, favoring the formation of strandplains. The presented study shows that erosional cheniers can form only when there is enough sediment availability to counteract wave action and for a specific range of shelf slopes.

## 1. Introduction

The word chenier derives from the Cajun name for oak, *chêne*, which is the prevalent tree encroaching sand ridges in southwestern Louisiana (Russell and Howe, 1935). In geomorphology, chenier is defined as a fossil sandy ridge amassed on muddy sediment and separated from the shoreline by a mudflat, formed by the deposition of fine cohesive littoral sediments (Byrne et al., 1959). The nature of the coastal ridges consists in deposits of sandy sediment, gravel or shell resting stratigraphically on mud (Otvos and Price, 1979). The aim of this work is to quantify how different sediment characteristics and wave climates can drive the stratigraphic genesis of the following three coastal landscapes: sandy strandplains, mudflats, or the alternate combination of the previous two formations, i.e. erosional chenier plains.

Previous studies have investigated chenier plains formation, without quantifying the key processes responsible for their occurrence. Chenier plains can be found in river deltas (Saito et al., 2000), in estuaries and bays, both in mesotidal or macrotidal systems (Otvos and Price, 1979; Woodroffe et al., 1983; Anthony, 1989; Park et al., 1996; Borrego et al., 2000; Morales et al., 2014). Draut et al., (2005) indicate that cheniers in Louisiana might have formed during strong storms in the presence of fluid muds and energetic wave climate. A recent study from Anthony et al., (2014) investigates the formation of one of the largest chenier plains system on Earth along the Guiana's coast of South America. These cheniers develop as a result of migration of mud banks from the mouths of the Amazon and Orinoco river deltas (Anthony et al., 2010; 2014).

In wave-dominated deltas, large ridge features form by wave-winnowing and remobilization of sand or shell fragments during energetic storms. In these settings muddy cohesive sediments cyclically separate a sandy-ridge system from the ocean with a development of a mudflat in front of the ridge. As a result, alternate ridges and mudflats, called erosional chenier plains, give rise to bands along the shoreline, as

49 found for instance in Louisiana (Draut et al., 2005) and in the Mekong delta (Tamura et al., 2012;  
50 Nardin et al., 2016).

51 In other deltaic conditions, spit ridges develop at the mouths of delta distributaries, sheltering erosional  
52 backwaters that are subsequently filled with mud. These depositional chenier plains are typical of the  
53 Danube (Bhattacharya and Giosan, 2003) and Rhone deltas (Kruit, 1955).

54 Cheniers can also form with mechanisms different from the erosional and depositional cases. For  
55 example, the Chenier plains studied by Anthony et al., (2010) near the mouth of the Amazon River  
56 form by spatial variations in wave energy induced by the alternations of mud banks migrating  
57 alongshore and separated by inter-bank areas.

58 In this work we only study the formation of erosional chenier plains, caused by the the remobilization  
59 during energetic storms of lag coarse sediments in muddy tidal flats.

60 Augustinus (1989) discussed the origin of erosional cheniers when muddy deposition at the shore is  
61 disturbed by a high energy events resulting in a sandy or shell deposit. However, this study did not  
62 quantify under what conditions this system form or modeled in detail the physical processes at play.

63 A different landform created by high energy waves is a strandplain, which is a broad accumulation of  
64 sand in parallel deposits or dunes along the shoreline (Hein et al., 2013; Otvos and Price, 1979).

65 Contrary to cheniers, strandplains are not separated by mud deposits. Here we will determine under  
66 what conditions a strandplain or an erosional chenier plain form at the shore.

67 Roy et al., (1994) determined that strandplains are frequent along coasts with high waves, rich in  
68 sediments, and facing wide and gentling sloping continental shelves. Strandplains and chenier plains  
69 are common landscapes worldwide (Franceschini and Compton, 2006). They are present in Australia  
70 on the gulf of Carpentaria (Chappell and Grindrod, 1984; Woodroffe and Grime, 1999; Harvey, 2006;  
71 Nott et al., 2009), in Egypt on the Nile delta (Goodfriend and Stanley, 1999) in Brazil (Hein et al.,  
72 2013), and along the West coast of Africa (Anthony, 1995).

In our study, we carried out a set of numerical simulations with the numerical models Delft3D (Lesser et al., 2004) and SWAN (Booij et al., 1999) to generate a database for a theoretical investigation on the formation of erosional chenier plains using dimensional analysis. The stratigraphic module of Delft3D is used to generate and record deposition of alternate sediment layers. The same numerical framework was recently used to explore the impact of waves on coastal morphology (Nardin & Fagherazzi, 2012; Nardin et al., 2013) and the effect of tides on the alternate deposition of mud and sand (Leonardi et al., 2014).

## **2. Dimensional Analysis**

Most published work focuses on chenier morphological and sedimentological characteristics around the world (Russell and Howe, 1935; Byrne et al., 1959; Augustinus, 1989). These studies address the physical mechanisms responsible for chenier genesis from a qualitative point of view. Our goal is to build a process-based rationale centered on dimensional analysis of numerical results.

As usually present in many chenier plain locations, we study a schematic case of a seaward slope in front of an approximately plane mudflat (Figure 1). This conformation refers to the broadly observed study case in which sediment resuspension by waves is capable of displacing the sediment stored at the shoreline.

Erosional chenier plain genesis can be divided in two main stages: formation of a sandy ridge and formation of a mudflat in front of the ridge. The dynamics of ridge formation depend on wave energy during extreme storms and the nature of the non-cohesive sediments present on the shelf. The initial seaward slope plays a crucial role in sediment winnowing and in the morphological response to wave action.

We assume that significant wave height,  $H_s$  (associated with a critical shear stress,  $\tau_{ws}$ , during storms event), and sediment characteristics (grain size,  $D_{50}$ , and density,  $\rho_s$ ) are the driving variables for the

97 development of the sandy (or shell gravel) ridge. The second stage of chenier formation is the  
 98 deposition and subsequent progradation of a mudflat in front of the sandy ridge during fair-weather  
 99 conditions. Mudflat formation mainly depends on the properties and availability of cohesive sediments,  
 100 dictated by concentration,  $c_m$  and settling velocity,  $w_s$ . Because the mudflat is subject to wave attack,  
 101 erosion from small, fair-weather waves is present during the mudflat formation cycle. We recognize the  
 102 importance of other two variables: wave bottom shear stress during fair-weather conditions,  $\tau_w$ , and  
 103 critical shear stress for mud erosion,  $\tau_{cr}$ , stating the predisposition of the bottom substrate to be  
 104 resuspended by waves. The list of relevant processes is completed by including erosion during extreme  
 105 storms that can considerably reduce the mudflat extension.  
 106 We have thus identified a list of variables indispensable to describe chenier formation during the two  
 107 stages of sand ridge formation and mudflat progradation: 1) basinward slope  $S$  [ $L L^{-1}$ ]; (2) sediment  
 108 density  $\rho_s$  [ $M L^{-3}$ ]; (3) mean diameter of sand or shell gravel  $D_{50}$  [ $L$ ]; (4) average cohesive sediment  
 109 concentration in the water column  $c_m$  [ $M L^{-3}$ ]; (5) critical shear stress for erosion  $\tau_{cr}$  [ $M L^{-1} T^{-2}$ ]; (6)  
 110 settling velocity of mud  $w_s$  [ $L T^{-1}$ ]; (7) wave bottom shear stress  $\tau_w$  (and  $\tau_{ws}$  in case of extreme storms)  
 111 [ $M L^{-1} T^{-2}$ ]; (8) erodability of mud deposits  $M_e$  [ $M L^{-2} T^{-1}$ ]; where length,  $L$ , time,  $T$ , and mass,  $M$ ,  
 112 are the fundamental units of the problem. We apply the Buckingham's theorem of dimensional analysis  
 113 (Langhaar, 1951) stating that the explanation of chenier genesis can be expressed in terms of 5 non-  
 114 dimensional parameters, which can be chosen among all potential couples of independent non-  
 115 dimensional groupings. We select the inner-shelf slope and a combination of the following 4 non-  
 116 dimensional groups:

$$\Pi_1 = S ; \Pi_2 = \frac{\tau_{ws}}{(\rho_s - \rho_w)gD_{50}} ; \Pi_3 = \frac{\tau_w}{\tau_{cr}} ; \Pi_4 = \frac{c_m w_s}{M_e} ; \Pi_5 = \frac{\Pi_4}{\Pi_3} \quad (1a,b,c,d,e)$$

118 where  $\Pi_2$  is the susceptibility of sandy sediments to resuspension during storms,  $\Pi_3$  is the susceptibility  
 119 of mud deposits to erosion during fair-weather events,  $\Pi_4$  is the ratio between fine-sediments potential  
 120 deposition and potential erosion.

121 The formation of sandy ridges is then defined by a relationship between the two non-dimensional  
 122 variables  $\Pi_1$  and  $\Pi_2$ .

$$123 \quad \frac{\tau_{ws}}{(\rho_s - \rho_w)gD_{50}} = f(S) \quad (2)$$

124 mudflat formation is described by  $\Pi_1$  and  $\Pi_5$ :

$$125 \quad \frac{c_m W_s}{M_e \frac{\tau_w}{\tau_{cr}}} = g(S) \quad (3)$$

126 while mudflat erosion during storms is dictated by  $\Pi_1$  and  $\Pi_3$ :

$$127 \quad \frac{\tau_w}{\tau_{cr}} = h(S) \quad (4)$$

128 where  $f(S)$ ,  $g(S)$ , and  $h(S)$  are unknown functional relationships to be determined through numerical  
 129 experiments. It is important to note that equations (2), (3), and (4) were directly derived from the  
 130 definition of the principal variables and from the theorem of Buckingham.

### 131 **3. Numerical model**

#### 132 **3.1 Model description**

133 Chenier plains evolution is investigated coupling the computational fluid dynamics model Delft3D with  
 134 the wave simulator SWAN. Delft3D resolves the bi-dimensional shallow-water equations, using the  
 135 computed velocity field to determine geomorphological evolution. The generation and propagation of  
 136 waves in shallow water is computed by SWAN. Delft3D solves the continuity equation and the  
 137 horizontal momentum equations, using a turbulence closure method. Vertical accelerations are not  
 138 taken into account, because they are supposed to be small compared to the gravitational acceleration.  
 139 The vertical momentum equation is therefore approximated to the hydrostatic pressure relation (Lesser  
 140 et al., 2004).

141 Bedload and suspended transport of cohesive and non-cohesive sediments are modeled by the sediment  
142 transport and morphology modules. The Van Rijn (1993) formulation is used to calculate bedload  
143 transport. Suspended-load transport is modeled with the 3-dimensional diffusion-advection formulation  
144 with the sediment eddy diffusivity and viscosity set at the same value. The vertical eddy viscosity  
145 applies the standard  $k$ - $\epsilon$  closure formulation (Rodi, 1984) for all runs. A large eddy simulation  
146 technique is used to account for the horizontal eddy viscosity. SWAN can mimic random, short-crested  
147 waves in the open ocean and in shallow water regions. The key processes incorporated in SWAN are:  
148 wave-wave interactions, wave refraction, and wave dissipation. The dissipation term includes bottom  
149 friction (Hasselmann et al., 1973), whitecapping (Komen et al., 1984), and wave breaking (Battjes and  
150 Janssen, 1978).

151 Our runs are planned to explore the hydrodynamic and morphological settings of waves with different  
152 energy levels propagating into a coastal region with variable slope. We also explore the presence of  
153 sediments with different characteristics. Because chenier plain genesis is complex, we have limited our  
154 investigation to two different wave energy levels and two sediment types. In the first stage, ridge  
155 formation, high energy waves attack the mudflat, which has a small fraction of sandy sediments. Storm  
156 waves of short duration partially erode the mudflat. At the same time, waves and related wave setup  
157 wash over the sandy sediments accumulating them at the shore and thus forming a sandy ridge. In the  
158 second stage of chenier formation, mudflat extension, a low and constant wave energy coupled with  
159 high concentrations of cohesive sediments is assumed, such that waves can carry and deposit the  
160 sediments on the mudflat without eroding the substrate.

161

### 162 **3.2 Numerical model set-up and simulations**

163 We present modeling results on how waves and sediment characteristics can drive the process of  
164 chenier plain formation in a rectangular basin with rectangular cells, whose long cell dimension is

165 along the coast (Fig. 1a). The grid has 50 by 50 computational cells, each of size of 100x20 m and it is  
166 finer along the cross-shore direction to better model wave propagation. Model runs are divided in two  
167 parts: chenier formation and mudflat establishment. Both use the same domain but with different  
168 sediments, waves, and basin slopes.

169 We start from a mudflat with a 10% sand content and a constant slope. We then apply a storm  
170 event, which erodes part of the mudflat and generates an accumulation of sandy sediments at the shore.  
171 Afterward, fair-weather conditions are simulated resulting in the formation of a new mudflat in front of  
172 the ridge. The run is then stopped and restarted with the same bed level configuration but replenishing  
173 the initial content of sand in the sediment deposited in the mudflat (10%). This allows to always have  
174 available sand in the shelf sediments to build a new chenier. A new storm event is then generated. After  
175 several runs a new chenier forms. We simulate two-day storm every ten years, then ten years for  
176 mudflat progradation with fair-weather waves.

177 The basin has an initial slope between 0.004 and 0.013 along the east-west direction, creating an  
178 initial water depth at the West boundary between 6 and 20 m. The initial bed level is planned to  
179 represent an initial mudflat configuration. A white-noise perturbation between 0 and 5 cm is  
180 superimposed to the bottom elevation to simulate the natural variability of the shelf substrate.  
181 Sensitivity tests show that the shoreline extension in both directions of the computational domain does  
182 not change the results of the study. The North, South, and East boundary conditions are zero elevation  
183 water level (Figure 1). A five meters deep layer of mixed cohesive and non-cohesive sediments is  
184 originally accessible for erosion at the bottom of the domain.

185 We first carry out 164 simulations with negligible equilibrium concentrations of non-cohesive  
186 sediments at all boundaries. We use three diameters,  $D_{50}$ , for the sand fraction (100, 200 and 1,000  
187  $\mu\text{m}$ ). The specific density of the sediment is  $2,650 \text{ kg m}^{-3}$ , while the dry density of the bed is  $1,600$   
188  $\text{kgm}^{-3}$ . Characteristics of the cohesive sediment are chosen in agreement with values provided by



189 Berlamont (1993). Specific density is  $2,650 \text{ kgm}^{-3}$ , dry bed density is  $500 \text{ kgm}^{-3}$ , settling velocity varies  
190 from  $0.05 \text{ mm s}^{-1}$  to  $0.5 \text{ mm s}^{-1}$ , and cohesive sediment concentrations of  $0.4$  and  $1.0 \text{ kg m}^{-3}$ .

191 In case of cohesive sediments, the Partheniades–Krone formulation for erosion and deposition are  
192 used (Partheniades, 1965). In this formulation, the critical shear stress for erosion is always greater than  
193 or equal to that for deposition. The horizontal eddy-viscosity coefficient is defined as the combination  
194 of the subgrid-scale horizontal eddy-viscosity, computed from a horizontal large-eddy simulation, and  
195 the background horizontal viscosity here set equal to  $0.001 \text{ m}^2 \text{ s}^{-1}$ . We used a morphological factor of  
196 500 to speed-up our model runs, after we define that the final result was not influenced.

197 Wave parameters ( $H_s$  and  $T_p$ ) are selected to simulate waves generated in the ocean. We vary  $H_s$   
198 between  $0.1\text{m}$  and  $3\text{m}$ , and use a period,  $T_p$  of  $5\text{s}$  during mild-weather conditions and  $10\text{s}$  during  
199 storms. In order to investigate the sandy ridge formation with the higher slope of  $S=0.013$ , we model  
200 highly energetic waves with  $H_s=4\text{m}$ . We impose wave period and significant wave height at the East  
201 boundary, orthogonal to the shoreline avoiding any major alongshore current development. Wave  
202 reflection is not accounted for in the wave model so that wave energy is dissipated at the coastline.

203

#### 204 **4. Results and discussion**

205 As a first result, we plot  $\frac{\tau_{ws}}{(\rho_s - \rho_w)gD_{50}}$  versus  $S$  in Fig. 2a, which, based on equation (2), offers a  
206 characterization of  $f(S)$ . We find that the formation of a sandy ridge for different wave heights and  
207 grain sizes depends on bottom slope. For high slopes (larger than  $0.015$ ) it is always hard for waves to  
208 build a sand ridge. Therefore, a threshold in  $S$  exists above which ridge formation is prevented.  
209 We then study the impact of the percentage of sand in bottom sediments on ridge formation. Results  
210 with a sand percent of  $10\%$  and  $25\%$  do not differ. We therefore plot only the results with  $10\%$  of sand  
211 in our figures. During storms, waves can remove and re-suspend the entire fine sediment fraction at the  
212 shelf bottom while the non-cohesive sediment is accumulated at the beach forming a sandy ridge.

213 To better understand the dynamics of ridge formation displayed in Figure 2a, we analyze in detail the  
 214 equations governing sediment transport of sand by waves. In SWAN (Booij et al., 1999) the waves  
 215 induced shear stress,  $\tau_w$  ( $\tau_{ws}$  in case of storms) is calculated as:

$$216 \quad \tau_w = \frac{1}{2} \rho f_w u_b^2, \quad u_b = \frac{\pi H_s}{T_p \sinh(KD)} \quad (5a,b)$$

217 where  $\rho$  is the fluid density,  $u_b$  is the wave bottom orbital velocity,  $H_s$  is the significant wave height,  $T_p$   
 218 is the wave peak period,  $D$  is the domain depth,  $K$  is the wave number, and  $f_w$  is a wave friction factor,  
 219 calculated as:

$$220 \quad f_w = \begin{cases} 0.00251 \exp \left[ 5.21 \left( \frac{u_b}{\omega k_s} \right)^{-0.19} \right] & ; \frac{u_b}{\omega k_s} > \frac{\pi}{2} \\ 0.3 & ; \frac{u_b}{\omega k_s} < \frac{\pi}{2} \end{cases} \quad (6)$$

221 where  $\omega$  is the angular frequency,  $k_s$  is the Nikuradse roughness, estimated as 3.5 times the median  
 222 sediment grain size,  $D_{50}$ . A more detailed discussion of the SWAN model can be found in the  
 223 supporting information (Grant and Madsen, 1979; Soulsby et al., 1993a).

224 From these equations an increase in median grain size of sand,  $D_{50}$ , leads to an increase in roughness,  
 225  $k_s$ , and consequently friction,  $f_w$ , while the bottom shear stress,  $\tau_w$ , decreases. As a result, there is less  
 226 erosion for large grain sizes. Moreover, from the Shields parameter a higher grain size requires a higher  
 227 bottom shear stress in order to mobilize the sediment. An increment in significant wave height  
 228 enhances the bottom orbital velocity, and therefore bottom shear stress,  $\tau_w$ . Consequently, higher  
 229 waves erode more sediment. The non-dimensional number  $\frac{\tau_{ws}}{(\rho_s - \rho_w)gD_{50}}$  therefore represents the potential  
 230 mobilization of bottom sediments (Shields parameter for waves).

231 Bottom erodibility also depends on inner-shelf slope, and an increasing in nearshore slope leads to a  
 232 narrow surf zone close to the beach. High slopes thus imply a reduced potential for sand entrainment on  
 233 the shelf (Figure 2a). This is the reason why for steep shelf slopes it is hard to erode sand from the

234 bottom and generate a sandy ridge. This is in accordance with Hein et al. (2013), who show that a low  
 235 shelf slope and high energy waves favor the formation of strandplain in Pinheira, southeastern Brazil.  
 236 The ratio between wave bottom shear stress,  $\tau_w$ , and critical shear stress for mud erosion,  $\tau_{cr}$ ,  
 237 represents the potential wave erosion of the mudflat.  $\tau_w$  is computed at the east boundary and strongly  
 238 depends on  $H_s$ . Our simulations show that the mudflat is preserved in the presence of weak waves or  
 239 very consolidated mud. By increasing the bottom slope, we decrease mudflat preservation, since  
 240 energetic waves break near the shore eroding the mud (Fig. 2a). On the contrary, a mild inner-shelf  
 241 slope favors wave energy dissipation across a wide area of the shelf, so that the incoming waves never  
 242 have enough energy to resuspend the muddy sediments.  
 243 Figure 2b displays the relationship between the non-dimensional variables controlling mudflat  
 244 formation and shelf slope. Our results show that for gentle slopes a high range of  $\Pi_5$  values lead to  
 245 mudflat formation while in steep inner-shelves it is difficult to deposit cohesive sediments. This is due  
 246 to a balance between deposition (at the numerator of the non-dimensional number  $\Pi_5$ ) and erosion by  
 247 waves (at the denominator). In fact, waves have a twofold effect, they move sediment to the shore  
 248 through wave-breaking and wave drift but they can also erode sediments from the bottom. Only when  
 249 the first process dominates you have mudflat formation.  
 250 In our runs, we want to grow a mudflat from the shore. Intermediate and high values of sediment  
 251 concentration can generate the initiation of a prograding mudflat. Low values of sediment  
 252 concentrations are not sufficient to overcome the mild wave erosion caused by fair-weather waves  
 253 (Figure 2b).  
 254 Potential mudflat erosion during storms is an additional important process during chenier plains  
 255 evolution. In our model simulations, if complete mudflat erosion occurs during a storm then a new sand  
 256 ridge is deposited in contact with the old ridge without mud deposits in between. In this case, we

257 classify the system as a strandplain, since the model would continue to deposit sandy ridges side by  
258 side leading to long-term progradation.

259 To better understand erosion by waves on a mudflat we analyze shelf elevations and maximum bed  
260 shear stress after storms for four numerical test cases (Figure 3). For a fixed wave peak period of 10s,  
261 mudflat erosion increases for higher wave heights and for lower shelf slopes (Figure 3a). Maximum  
262 bed shear stress with 3 m waves is four times higher than with waves of 1 m (Figure 3b) and maximum  
263 values are observed where waves break (Figure 3a). These results explain why in Figure 2a high values  
264 of  $H_2$  lead to sandy ridges by remobilizing large volumes of sand on the shelf. On the other hand, high  
265 values of  $H_2$  also lead to the erosion of a larger portion of mudflat (Figure 2b,  $H_3$  is directly  
266 proportional to wave shear stress).

267 All our results fall in three categories: formation of mudflat only, formation of an erosional chenier  
268 plain, and formation of a strand plain (Figure 4a). Inner-shelf slope drives the process of mudflat or  
269 ridge creation. We can produce an alternation of these two landforms (second column in Figure 4a) or  
270 simply continue with a mudflat progression (first column of Figure 4a). Moreover, if we erode the  
271 mudflat during each storm, we generate a strand plain composed of consecutive sandy ridges without  
272 mud deposits in between (third column in Figure 4a).

273 Storm energy and frequency are also important for chenier formation. If mud deposition does not have  
274 enough time to form an expansive mudflat, a storm can erode all the mud leaving only a sequence of  
275 sandy ridges (strandplain, third column of Figure 4a). We also explored the effect of storm frequency  
276 and sediment concentration on mudflat extension and preservation (Figure S1). The longer is the period  
277 between two extreme storms the wider is the mudflat depositing in front of the ridge. Periods without  
278 large storms lasting 100 years build a mudflat that is 4-6 times longer than a mudflat built in 10 years.  
279 Therefore, if extreme storms are less frequent, there is a higher chance to preserve the mudflat between  
280 ridges and form an erosional chenier plain rather than a strandplain. Here, for sake of simplicity, we fix

281 in each simulation a storm event frequency equal to one extreme event per 10 years. The remaining  
 282 time is dedicated to build a mudflat under different conditions of sediment supply (Figure 2b). Future  
 283 research will explore how the statistical distribution of storms and their inter-arrival times control the  
 284 formation of chenier plains. Although our model results explored a fixed storm interval, additional  
 285 modeling studies might be able to look at chenier plains formation as a time recorder of past storms  
 286 activity.

287 For a given choice of parameters, Figure 4b shows through a flow chart all the possible morphological  
 288 outcomes as a function of storms and deposition events. Storms with high energy are critical for the  
 289 formation of sand ridges, bringing sediment to the shore (Fig. 2a). If such storms are not present, only a  
 290 mudflat can form when the shelf slope is mild and cohesive sediments available. The lower is the cross-  
 291 shore slope, the more likely is the formation of a mudflat (Fig. 2c). A low slope also favors the  
 292 formation of a sand ridge, because waves can mobilize more sediment and move this material to the  
 293 shore. Intermediate slopes prevent the formation and preservation of a mudflat, so that only a  
 294 strandplain can form during storms. Finally, for high bottom slopes, neither a mudflat nor a sand ridge  
 295 form, and shore progradation is absent (Table 1).

	Low wave-energy during storms	High wave-energy during storms
Low cross-shore slope	Mudflat	Chenier-plain
Intermediate cross-shore slope	No progradation	Strandplain
High cross-shore slope	No progradation	No progradation

296 **Table 1 Formation of mudflats, chenier plains, and strandplains as a function of cross-shore**  
 297 **slope and wave energy during storms.**

298  
 299 Strandplains are typical of wave-dominated coasts where muddy sediments are resuspended and moved  
 300 offshore by waves. Offshore of muddy coasts with large sediment supply there is a clear subaqueous  
 301 slope-break, called roll-over point (Friedrichs and Wright, 2004; Eidam et al., 2017), which is  
 302 controlled by sediment inputs, sediment characteristics and waves. Here we model the inner part of the

shelf, onshore of the roll-over point. We therefore assume that the roll-over point is offshore of our studied area restricting the simulations to the top set of the subaqueous delta (Walsh and Nittrouer, 2009).

## 5. Conclusions

A non-dimensional analysis applied to a set of numerical simulations carried out with the numerical models Delft3D and SWAN sheds light on the genesis of erosional chenier plains. These landforms are characterized by the alternate deposition of two distinct units: sand ridges and mudflats. Sandy deposits are shaped by the action of waves but are mainly controlled by the inner-shelf slope. The amount of sand available at the shelf bottom plays a less important role, although at very low sand concentrations the ridge cannot form. Mudflat formation is dictated by sediment transport, accumulation, and erosion by waves, which depend on the following sediment parameters: settling velocity, sediment concentration in the water column, as well as critical shear stress for erosion. Gentle shelf slopes facilitate mudflat formation because high deposition rates overcome mild erosion by waves. The repetition of ridge and mudflat formation leads to the development of chenier plains (Figures 1b and 4a). However, depending on nearshore slope, a chenier plain may morph into a sequence of sandy beach ridges (strandplain) or a continuous mudflat losing the alternation between sand and mud. Our results provide a physically-based interpretation of the processes driving the formation of a chenier plain and partly explain why they are relatively uncommon along the shoreline (Table 1).

In order for an erosional chenier plain to form, cohesive sediments must be available in large volumes with enough sand or shell gravel that can be deposited during extreme events on the existing mudflat. During intense storms the mudflat can be eroded thus preventing the formation of a chenier system and favoring the establishment of a strandplain. Our results show that chenier genesis is less common because it depends on a specific balance between sediment availability and wave action.

327

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## 436 **Figure captions**

437 **Figure 1.** a) Computational domain and boundary conditions. Colors show bed levels in the domain  
438 and red arrows the wave direction. Central black dashed line shows the position of the control transect  
439 for the longitudinal profile sketch. b) Example of a cross-shore section of Chenier Plain formed from  
440 an initial mudflat with sand content of 25%. Colors show sand fraction in the deposited sediments (red  
441 is sand while blue is mud). Black lines indicate different profiles of the Chenier plain during evolution.  
442 c) Aerial photographs of Louisiana coastline nearby Atchafalaya river delta, LA, USA. Image Landsat,  
443 courtesy of Google Earth, Image 2013 Terra-Metrics.

444 **Figure 2.** (a) Relationship between the dimensionless significant waves height,  $\frac{\tau_{ws}}{(\rho_s - \rho_w)gD_{50}} = \frac{H_s}{D_{50}}$   
445 imposed at the East boundary and the inner-shelf slope,  $S$  with the red line and crosses. Black line  
446 shows dimensionless mudflat erosion as a function of inner-shelf slope. (b) Dimensionless mudflat  
447 deposition as a function of shelf slope (with  $M_e = 10^{-5}$ ). Black lines separate the area where a mudflat  
448 forms from the area where only a sandy ridge is present. Black and red lines in (a) and (b) plots show a  
449 transition between two geomorphic configurations as a function of basin slope,  $S$ . Circles with letters  
450 represent values of different coastal formation from study cases available in literature (see  
451 supplemental material).

452 **Figure 3.** Evolution of the cross-shore bottom profile for two different initial slopes (solid lines). Each  
453 initial slope is subjected to two different wave climates. Dashed lines represents the final bottom profile  
454 with  $H_s=1\text{m}$ , while dashed and dotted lines are relative to  $H_s=3\text{m}$ . b) Maximum bed shear stress along  
455  $x$  offshore direction at the  $y$  centerline. Bed sediment in the runs is composed by 90% of cohesive  
456 material with  $w_s=0.1\text{ mm/s}$  and  $\tau_{cr}=1\text{ Pa}$  and 10% of non-cohesive sediment with  $D_{50}=100\mu\text{m}$ .

457 **Figure 4.** a) Snapshots from 3 model runs showing longitudinal evolution, along the control transect in  
458 Figure 1a, of a prograding shoreline with different initial slopes under different wave climates and

459 sediment supplies. Red color means 100% sand, blue color means only mud. Each series consists of  
460 four instants of a mudflat evolving for 10 years. Black dotted lines show the initial cross-shore profile  
461 after a severe wave attack. First column: Mudflat case with initial slope  $S=0.013$ ,  $c_m=0.4$  kg/l,  $w_s=0.5$   
462 mm/s,  $\tau_{cr}=1$  Pa,  $D_{50}=100$   $\mu$ m and  $H_s=1$ m. Second column: Chenier Plain case formed by a series of  
463 two sandy ridges separated by a mudflat with initial slope  $S=0.013$ ,  $c_m=0.4$  kg/l,  $w_s=0.5$  mm/s,  $\tau_{cr}=1$  Pa,  
464  $D_{50}=100$   $\mu$ m and  $H_s=2$ m. Third column: strand plain case with initial slope  $S=0.013$ ,  $c_m=0.4$  kg/l,  
465  $w_s=0.5$  mm/s,  $\tau_{cr}=0.5$  Pa,  $D_{50}=200$   $\mu$ m and  $H_s=3$ m. b) A combined model of mudflats, strandplain and  
466 chenier plain generation.









